

*Linear time delay systems*  
*from characteristic roots...*  
*...to stability charts*

Dimitri Breda

dbreda@dimi.uniud.it - <http://www.dimi.uniud.it/dbreda>

Dipartimento di Matematica e Informatica  
Università degli Studi di Udine

## Outline of talk

- Introduction to DDEs

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Research in collaboration with  
**R. Vermiglio** - Università di Udine  
**S. Maset** - Università di Trieste

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- mathematical formulation by **retarded functional differential equations (RFDEs)**



## DDEs intro: remember ODEs

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- let  $X = \mathbb{C}^m$
- let  $(t, y) \in D \subseteq \mathbb{R} \times X$  and  $f : D \rightarrow \mathbb{C}^m$  continuous. An ordinary differential equation (ODE) is a relation

$$y'(t) = f(t, y(t)), \quad t \geq t_0$$

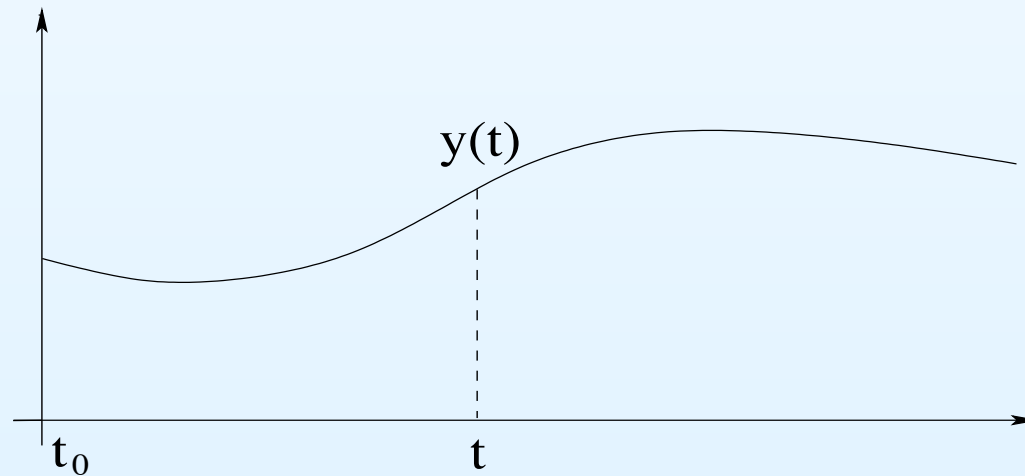
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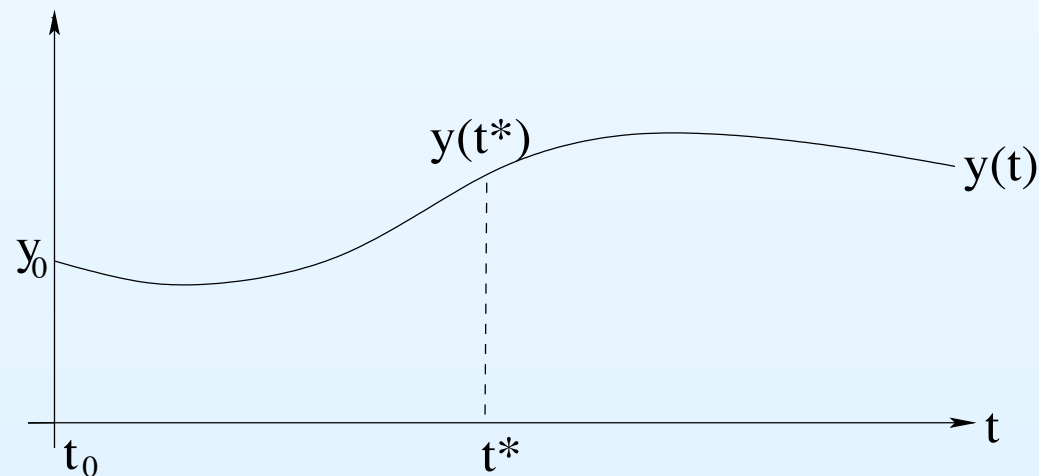
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- state  $y(t^*) \in X$  at  $t^* \geq t_0$  is **finite** dimensional and depends on initial **vector**  $y_0 \in X$ :



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- let  $\tau \geq 0$  and  $X = \mathcal{C}([- \tau, 0], \mathbb{C}^m)$
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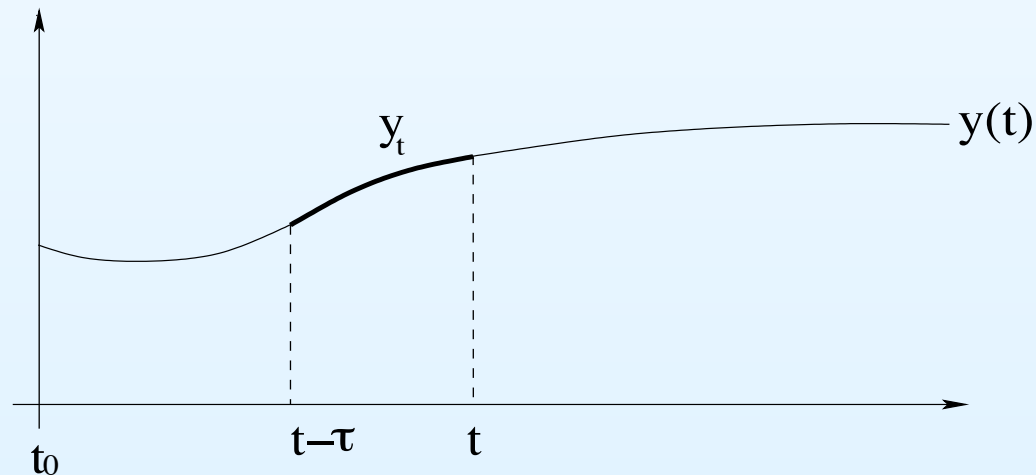
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- state  $y_t \in X$  at  $t \geq t_0$ :  $y_t(\theta) = y(t + \theta)$ ,  $\theta \in [-\tau, 0]$



## DDEs intro: examples

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- **discrete delay:**  $f(t, \psi) = L_0\psi(0) + L_1\psi(-\tau)$ , then for  $\psi(\theta) = y_t(\theta)$  on  $[-\tau, 0]$ :

$$y'(t) = L_0y(t) + L_1y(t - \tau)$$

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- **distributed delay:**  $f(t, \psi) = L_0\psi(0) + \int_{-\tau}^0 M_1(\theta)\psi(\theta)d\theta$ ,  
then for  $\psi(\theta) = y_t(\theta)$  on  $[-\tau, 0]$ :

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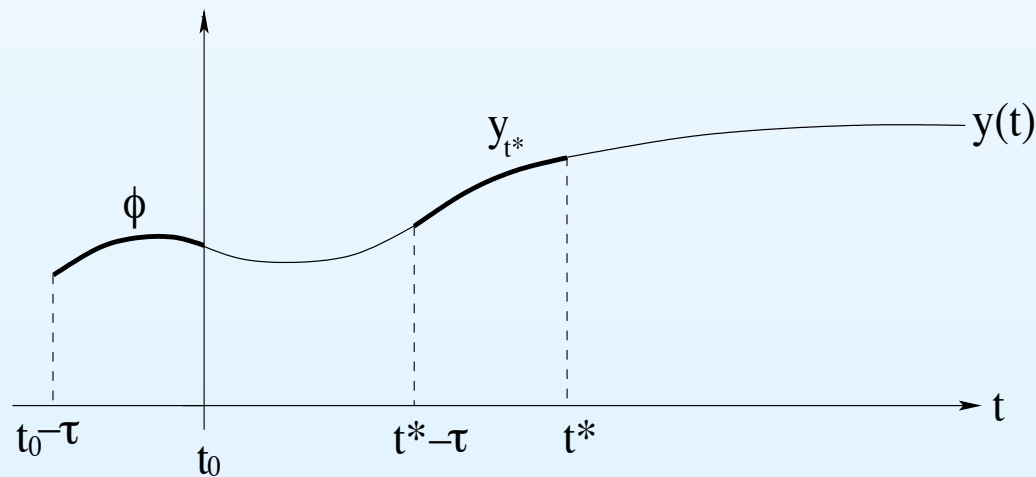
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$$\det(\lambda I - L) = 0 \Leftrightarrow \lambda \in \sigma(L)$$

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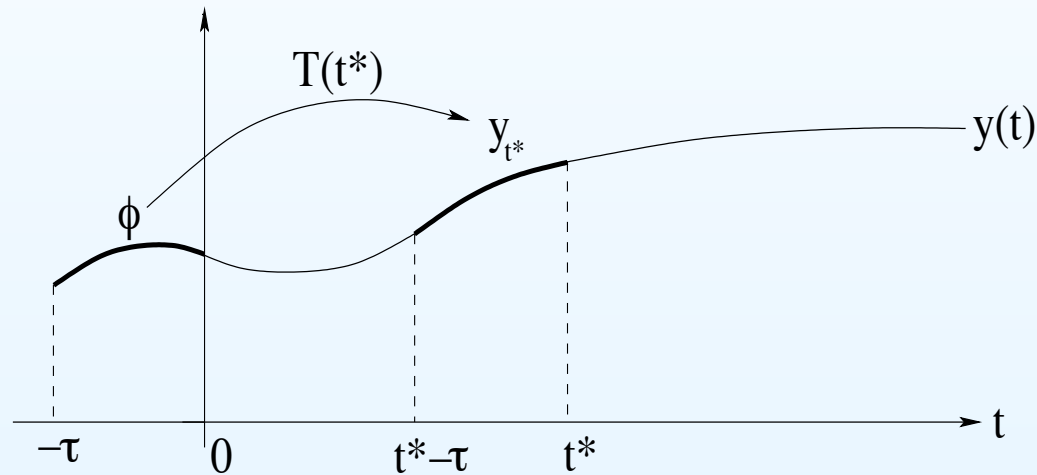
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- answer: YES!

## Stability: solution operator semigroup

- define solution operator (SO)  $T(t) : X \rightarrow X, t \geq 0$ :

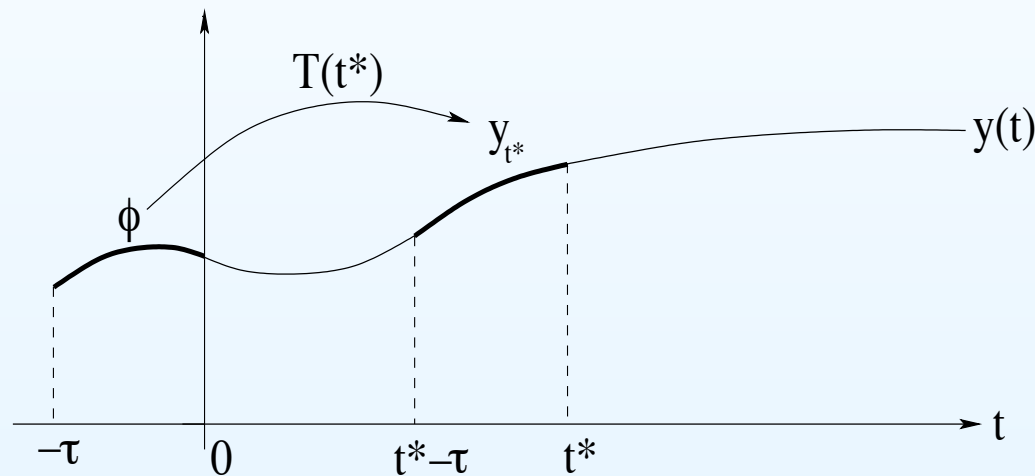
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- $\{T(t)\}_{t \geq 0}$  is a  $\mathcal{C}_0$ -semigroup

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- evolution of  $y_t$  depends on eigenvalues of  $\mathcal{A}$



## Stability: theorems

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- $\lambda \in \mathbb{C}$  **CR**  $\Leftrightarrow \det (\lambda I - L_0 - L_1 e^{-\lambda\tau}) = 0$
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- past: linear multistep (LMS) and Runge-Kutta (RK) methods
- present: pseudospectral differentiation (PSD)

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- Lagrange representation of  $\psi_N$  leads to...

## Numerics: approximated IG

---

...

$$\mathcal{A}_N = \begin{pmatrix} L_0 & 0 & \cdots & 0 & L_1 \\ d_{10} & d_{11} & \cdots & d_{1N-1} & d_{1N} \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ d_{N0} & d_{N1} & \cdots & d_{NN-1} & d_{NN} \end{pmatrix} \in \mathbb{C}^{m(N+1) \times m(N+1)}$$

where  $d_{ij} = l'_j(\theta_i) \otimes I$  with  $l_j$ 's the Lagrange coefficients

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- analogous result for CMs

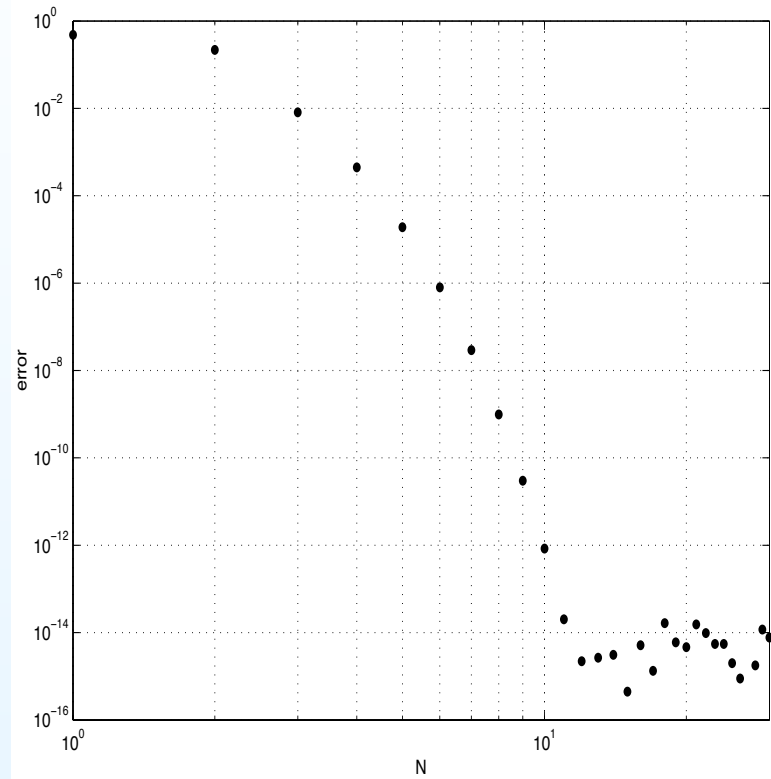
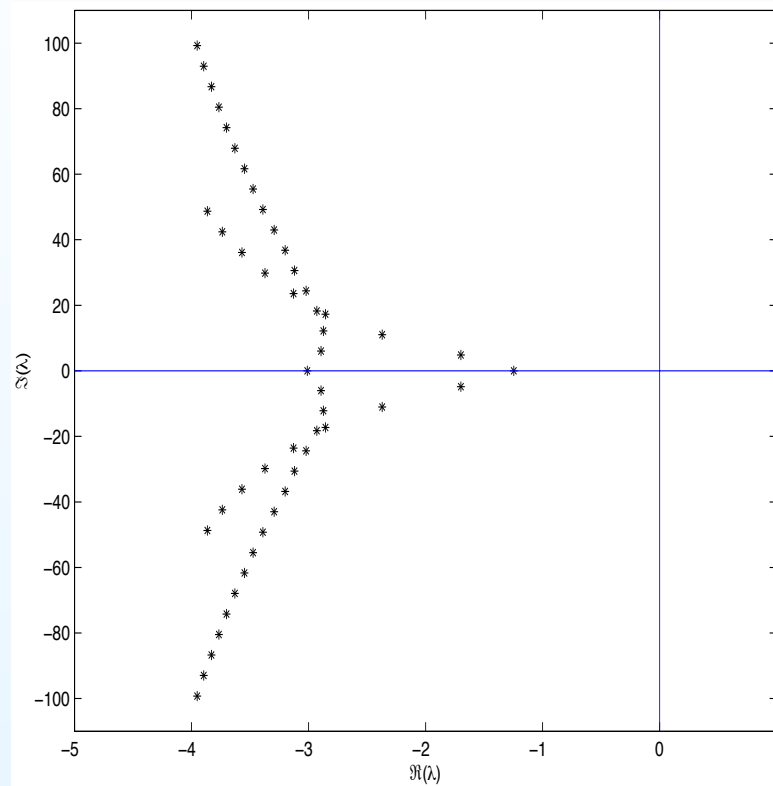
## Numerics: example

$$x'(t) = L_0x(t) + L_1x(t-1) + \int_{-0.3}^{-0.1} M_1x(t+\theta)d\theta + \int_{-1}^{-0.5} M_2x(t+\theta)d\theta$$

$$L_0 = \begin{pmatrix} -3 & 1 \\ -24.646 & -35.430 \end{pmatrix}, \quad L_1 = \begin{pmatrix} 1 & 0 \\ 2.35553 & 2.00365 \end{pmatrix}$$

$$M_1 = \begin{pmatrix} 2 & 2.5 \\ 0 & -0.5 \end{pmatrix}, \quad M_2 = \begin{pmatrix} -1 & 0 \\ 0 & -1 \end{pmatrix}$$

# Numerics: example



## Numerics: generalization

---

- linear multiple discrete/distributed DDEs:

$$y'(t) = L_0 y(t) + \sum_{l=1}^k \left( L_l y(t - \tau_l) + \int_{-\tau_{l-1}}^{-\tau_l} M_l(\theta) y(t + \theta) d\theta \right)$$

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- but also extension to more general **linear time delay systems (LTDS)**:
  - neutral DDEs
  - periodic coefficients DDEs
  - age-structured population dynamics
  - mixed-type FDEs
  - PDEs with delay

## Stability charts: what?

---

- consider a LTDS depending on two parameters  $p_1$  and  $p_2$  (e.g. delays, but not only...) varying in given intervals
- determine where the system is stable or not in the  $(p_1, p_2)$ -plane
- how?



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- how?
  - point-by-point investigation of the  $(p_1, p_2)$ -plane determining the real part of the rightmost CR  $r_{CR}(p_1, p_2)$  (or the absolute value of the dominant CM  $d_{CM}(p_1, p_2)$ )
  - also other approaches...

## Stability charts: example

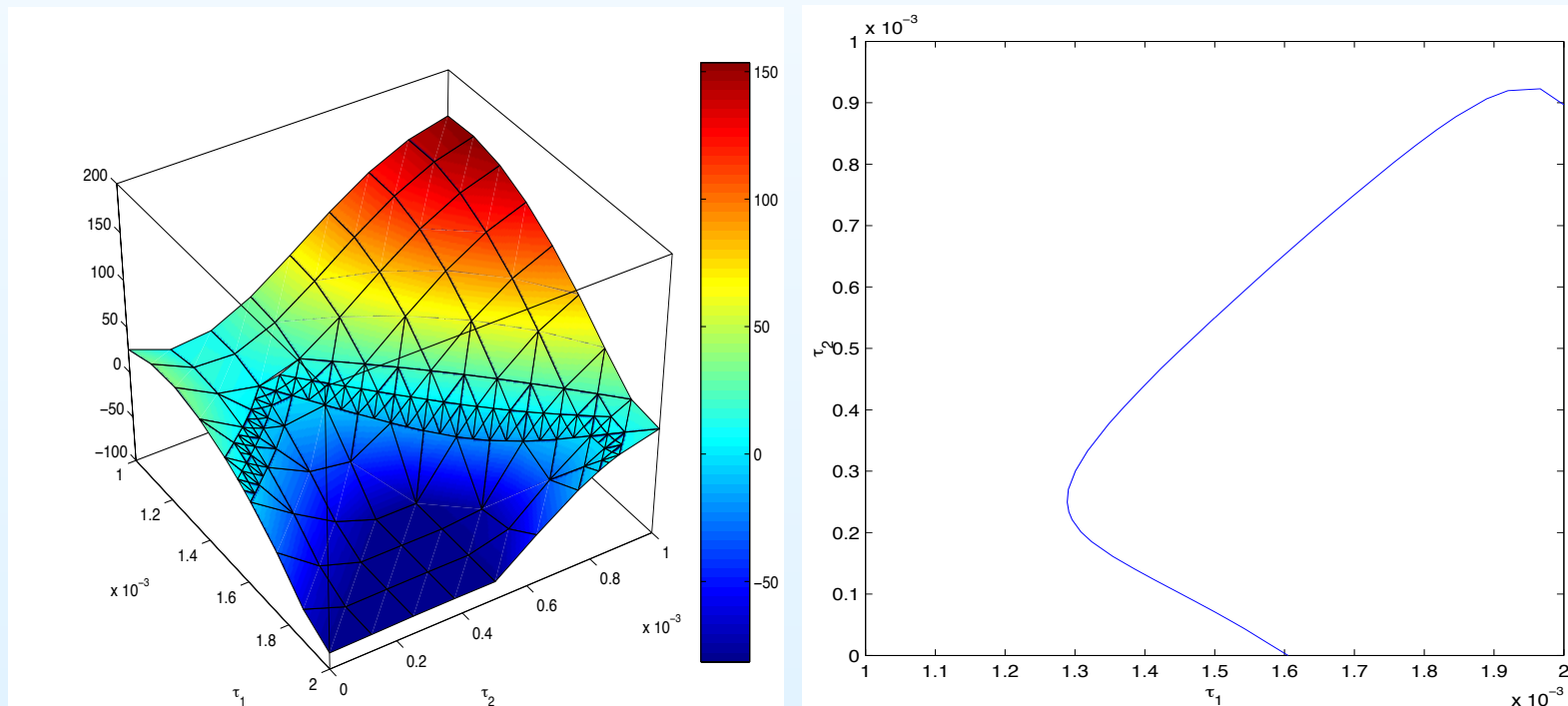
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A **stability boundary (SB)** is a curve  $r_{CR}(p_1, p_2) = 0$

## Stability charts: example

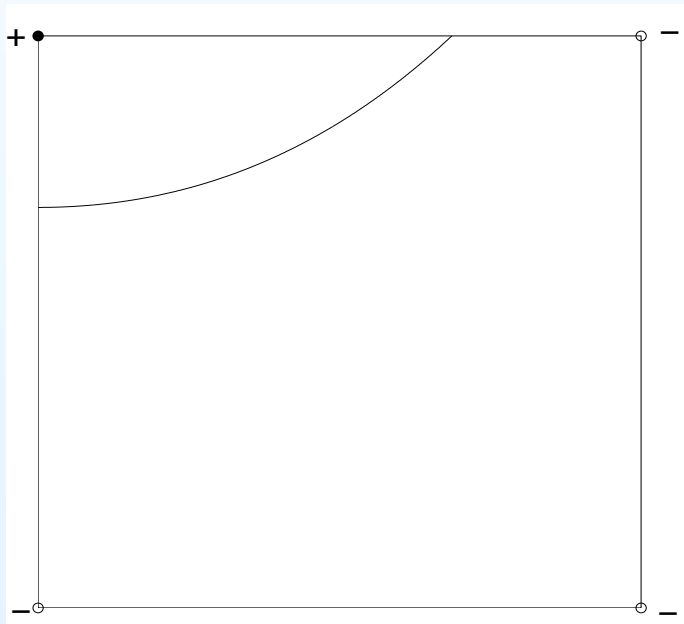
A **stability boundary (SB)** is a curve  $r_{CR}(p_1, p_2) = 0$

$$y'(t) = L_0 y(t) + L_1 y(t - \tau_1) + L_1 y(t - \tau_2) + L_2 y(t - 2\tau_1) + L_2 y(t - 2\tau_2) + L_3 y(t - \tau_1 - \tau_2), \quad L_i \in \mathbb{C}^{8 \times 8}$$



## Stability charts: point-by-point investigation

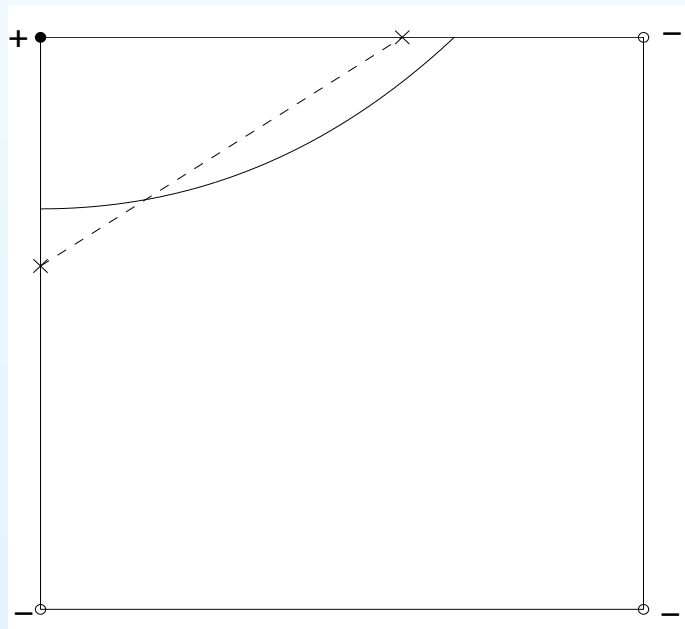
- consider a square **cell** in the  $(p_1, p_2)$ -plane
- evaluate stability of the four vertices by computing  $r_{CR}$
- if a **sign change** occurs, a SB passes through the cell



- a sort of  $2d$ -bisection

## Stability charts: location of SB

- consider **edges** with sign change in  $r_{CR}$  at the vertices
- for each edge, determine the point  $(p_1, p_2)$  such that  $r_{CR}(p_1, p_2) = 0$  by linear interpolation of vertex values
- approximate SB by joining the zeros



## Stability charts: uniform square grid

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- set a uniform square grid on the  $(p_1, p_2)$ -plane
- determine SB on each cell
- accuracy of SB depends on the grid size

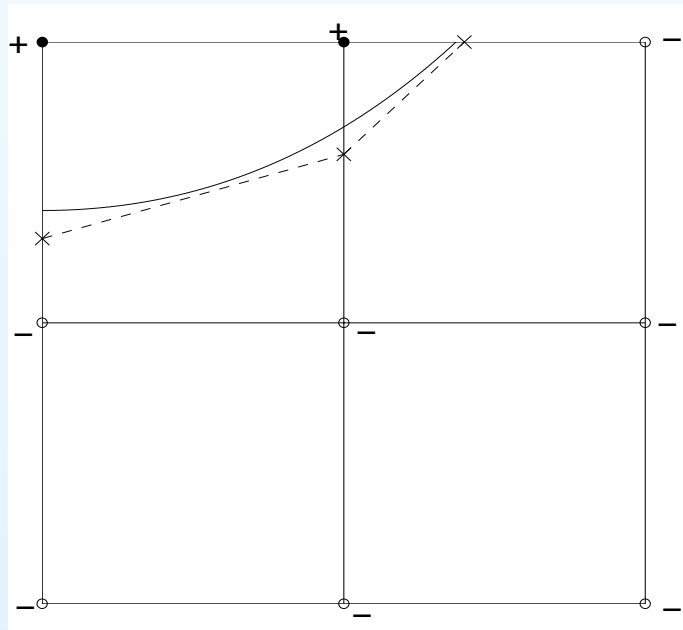
## Stability charts: uniform square grid

---

- set a uniform square grid on the  $(p_1, p_2)$ -plane
- determine SB on each cell
- accuracy of SB depends on the grid size
- this is behind *MATLAB's contour* for surface level-curves
- not efficient: each stability evaluation is **expensive**, hence uniform grid is not a good choice

## Stability charts: adaptive square refinement

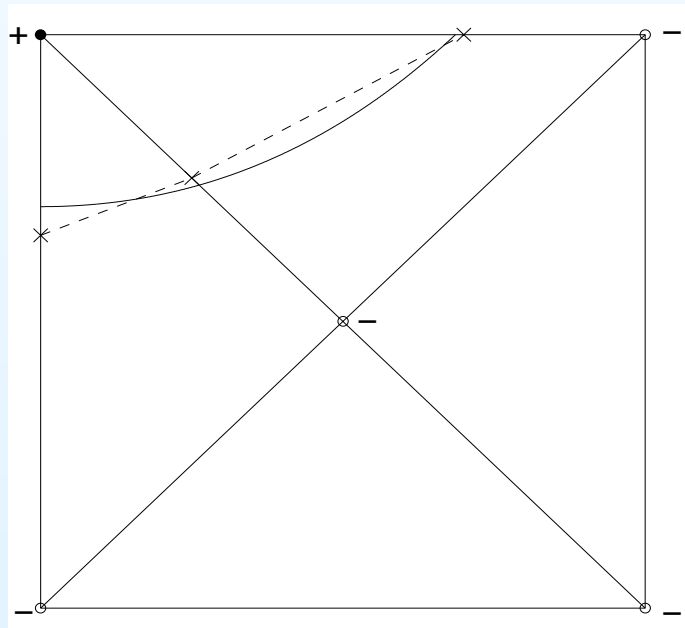
- start from a coarse square grid
- refine only cells with sign change by dividing into four square cells by the center point
- five new stability evaluations required





## Stability charts: adaptive triangulation 1

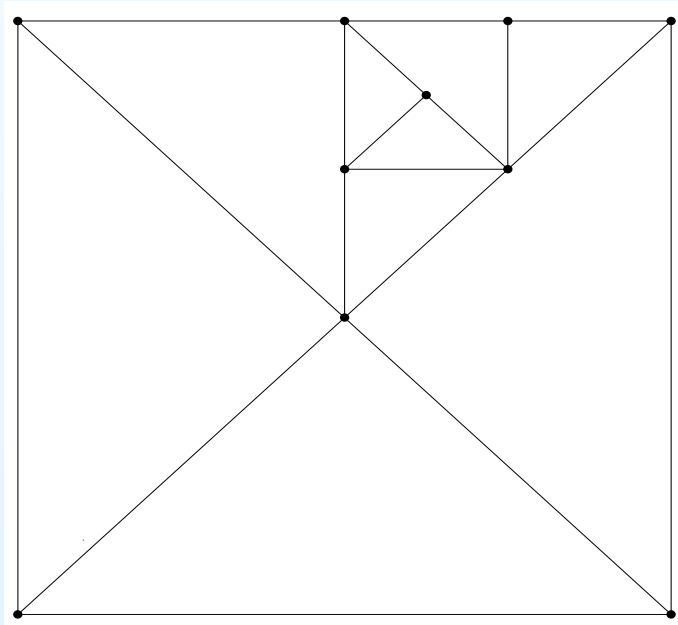
- start from a coarse square grid
- refine square cells with sign change by dividing into four triangular cells by the center point
- only one new stability evaluation required



## Stability charts: adaptive triangulation 2

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- start from a triangular cell with sign change
- refine by dividing into two triangular cells by the mid point of the hypotenuse
- only one new stability evaluation required



## Stability charts: squares vs triangles

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- start from a square with area  $A$
- consider the number of stability evaluations necessary to reduce the area to  $a$

## Stability charts: squares vs triangles

---

- start from a square with area  $A$
- consider the number of stability evaluations necessary to reduce the area to  $a$
- using square refinement

$$n = \frac{5}{\log 4} \log \frac{A}{a}$$

- using triangulation

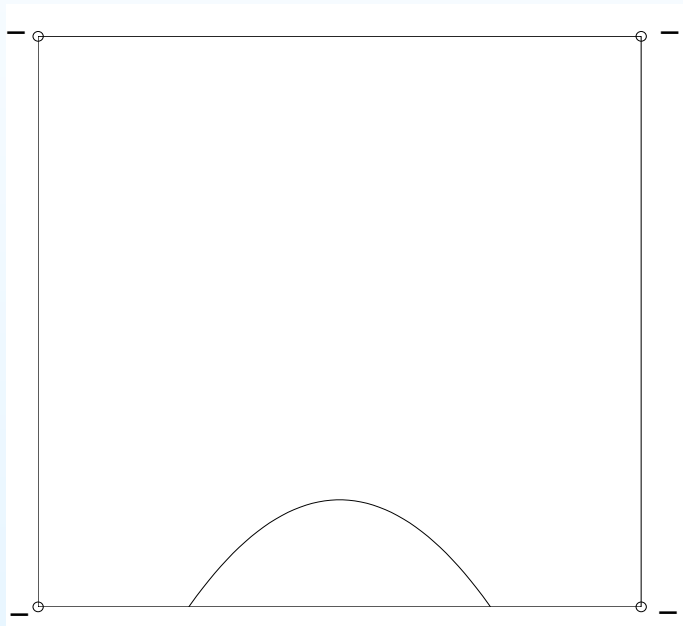
$$n = \frac{2}{\log 4} \log \frac{A}{a} - \log 4$$

- less than half!

## Stability charts: if no sign change?

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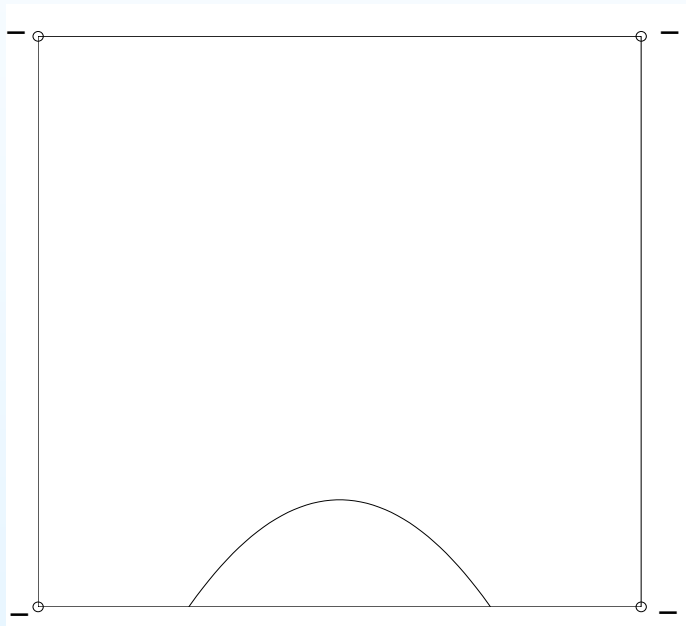
- if all vertices of a cell have same sign there might be a SB crossing the cell (at only one edge)



## Stability charts: if no sign change?

---

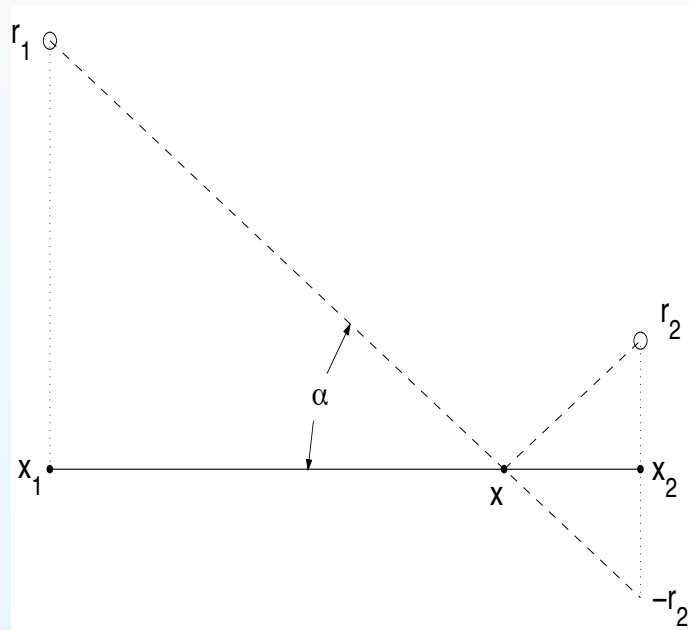
- if all vertices of a cell have same sign there might be a SB crossing the cell (at only one edge)



- how to recognize this possibility?

## Stability charts: slope test

- measure the minimum slope  $s = \tan \alpha = \frac{|r_1+r_2|}{|x_2-x_1|}$  at which  $r_{CR} = 0$  is reached from both edge vertices



- if  $s$  is too large exclude refinement, else refine
- not a sufficient condition: **heuristic test**

## Stability charts: multiple evaluations

---

- possible multiple evaluations for neighboring cells
- considerable increase of computational time: **not to underestimate**



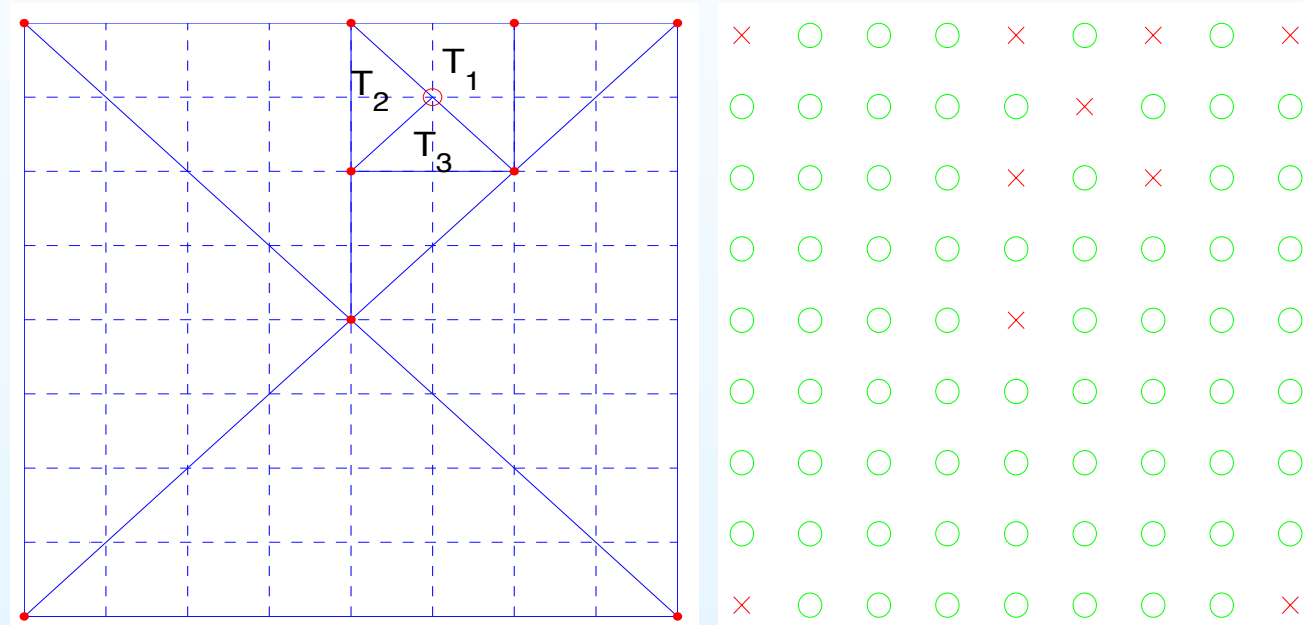
## Stability charts: multiple evaluations

---

- possible multiple evaluations for neighboring cells
- considerable increase of computational time: **not to underestimate**
- “easy” to avoid for square grid by storing stability information in a rectangular matrix with entries corresponding to grid points
- before evaluating a grid point check the matrix if it already exists

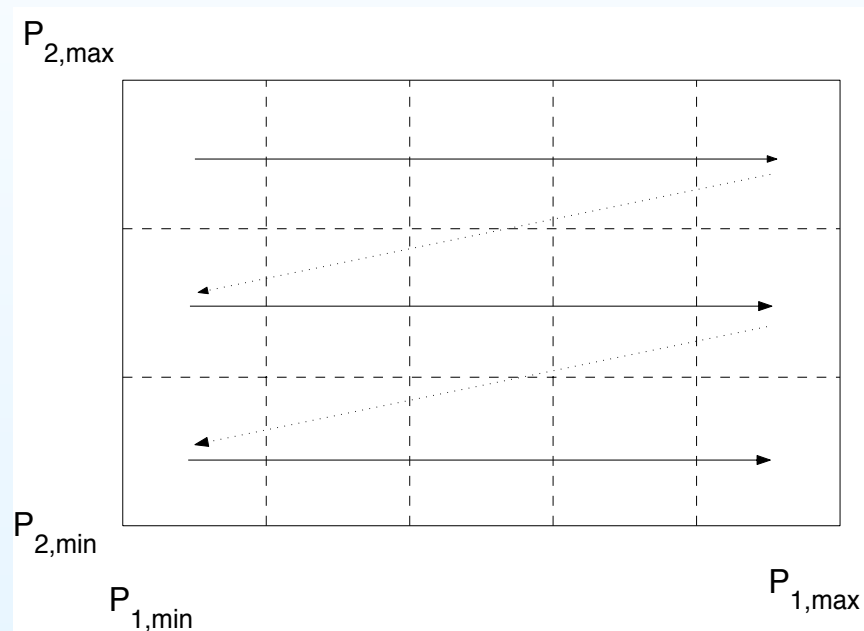
# Stability charts: information storage

- more difficult with triangulation
- use a square matrix for each square cell



## Stability charts: information passing

- update matrix from square to square scanning the whole grid in the usual reading/writing sense



- avoid multiple evaluations in each step!

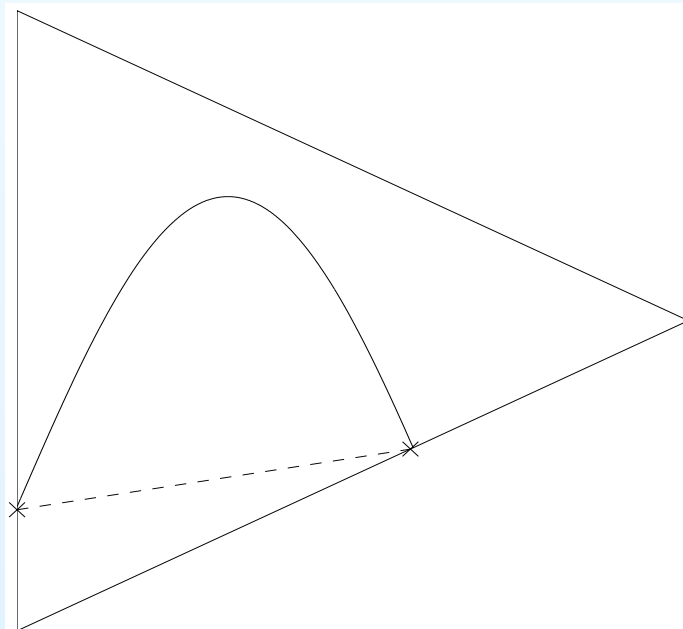
## Stability charts: location of SB

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- improve using **secant method** on each edge
- better control of accuracy along the edge

## Stability charts: location of SB

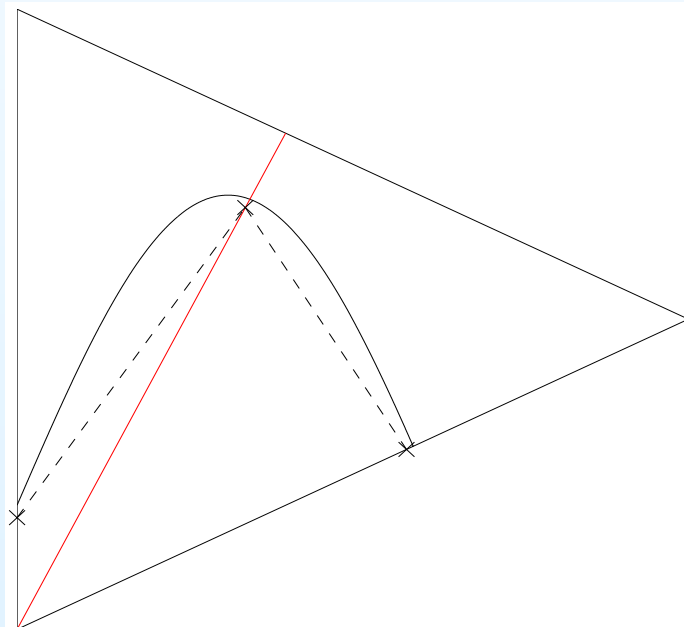
- improve using **secant method** on each edge
- better control of accuracy along the edge
- but...no sense in find zeros with high accuracy and then join them with a line: curvature of SB is determining



## Stability charts: adaptive curvature determination

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- take an extra mid edge and find its zero
- measure the height of the triangle formed by the zeros of the three edges
- if this height is too large, refine by an extra mid edge and iterate

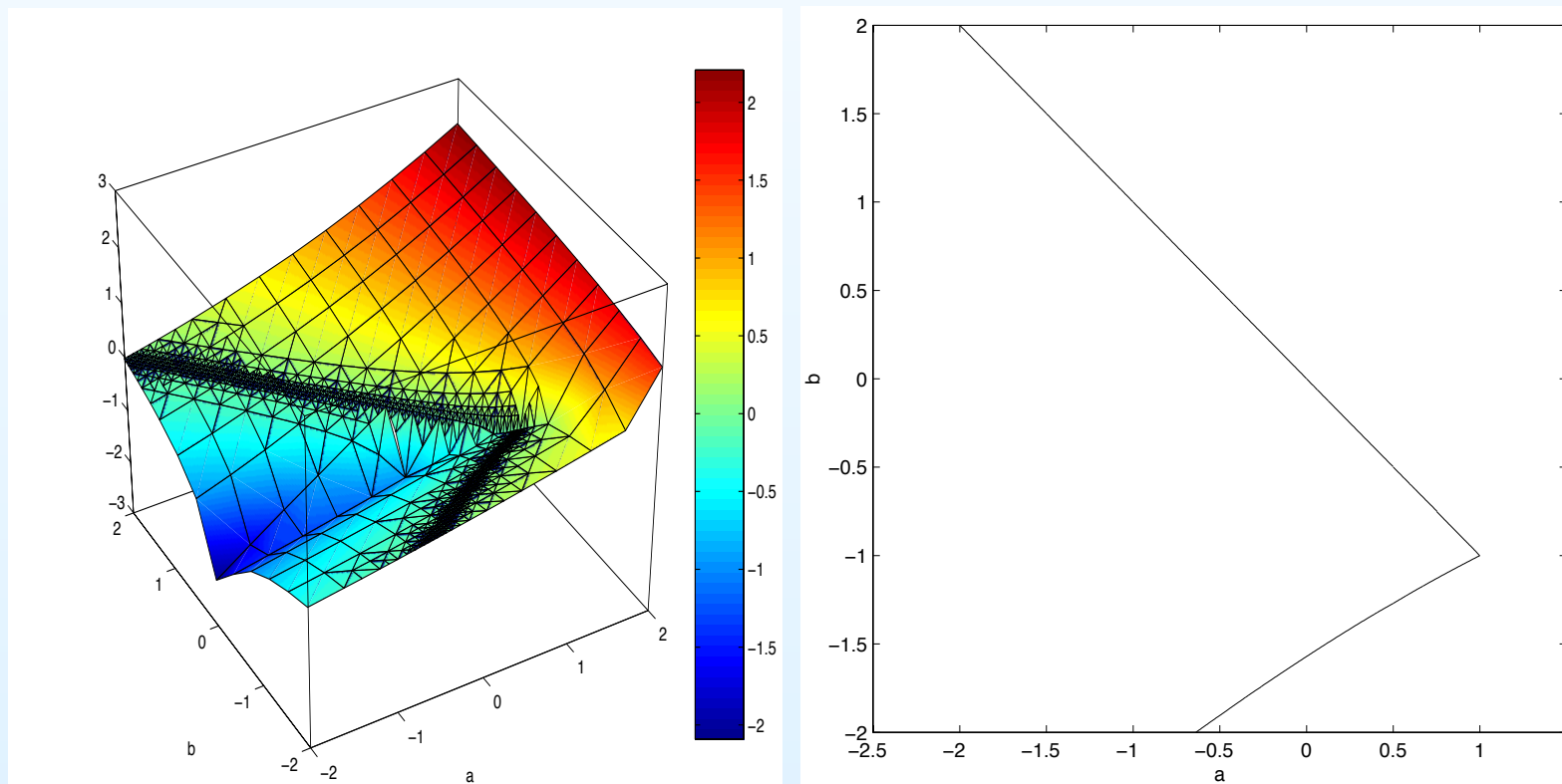


## Examples: single delay

- consider the scalar single DDE

$$y'(t) = ay(t) + by(t - 1)$$

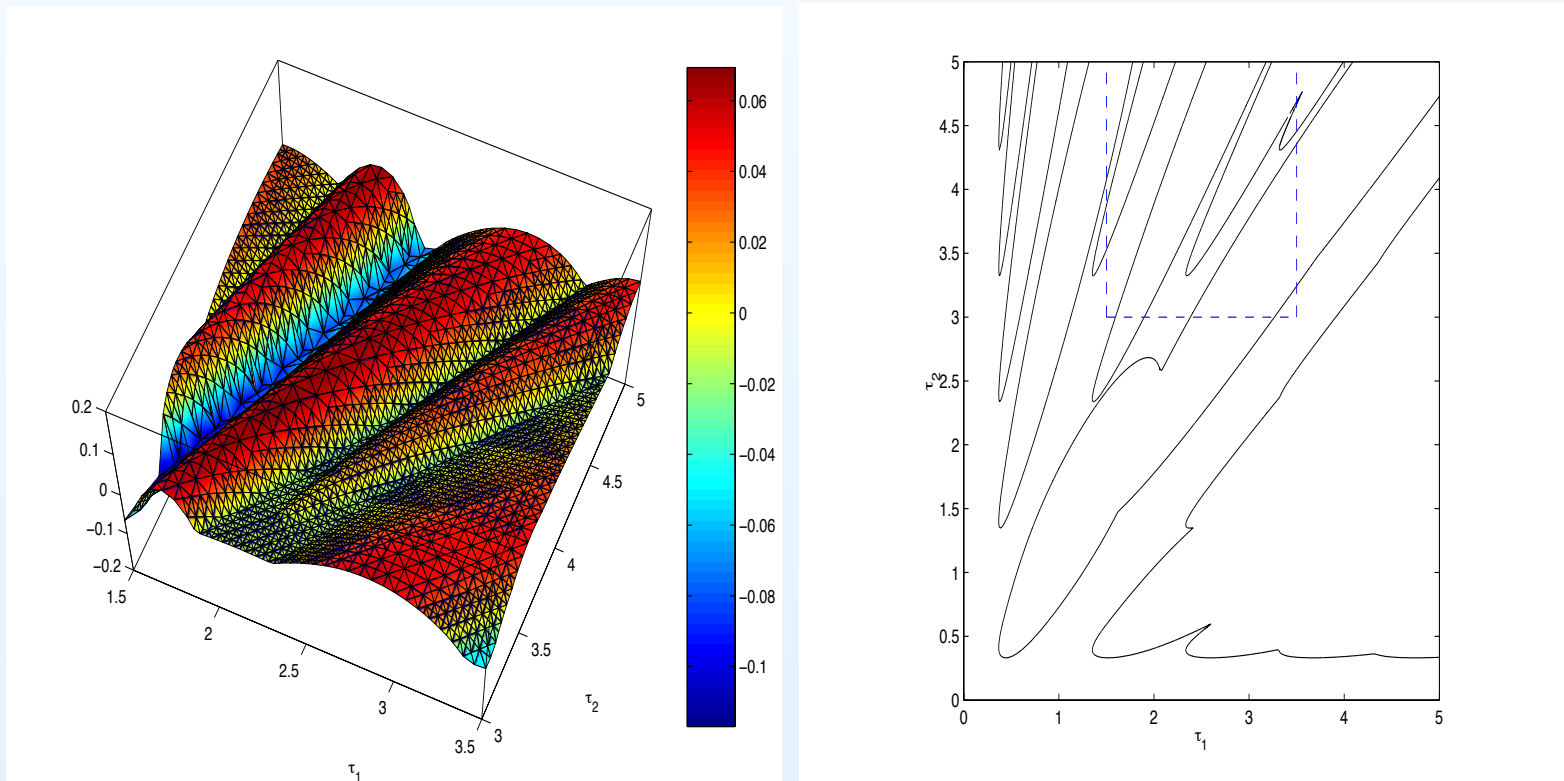
- stability chart analytically well-known



## Examples: multiple delays

- consider the 2d DDE

$$y'(t) = \begin{pmatrix} -6.45 & -12.1 \\ 1.5 & -0.45 \end{pmatrix} y(t) + \begin{pmatrix} -6 & 0 \\ 1 & 0 \end{pmatrix} y(t-\tau_1) + \begin{pmatrix} 0 & 4 \\ 0 & -2 \end{pmatrix} y(t-\tau_2)$$

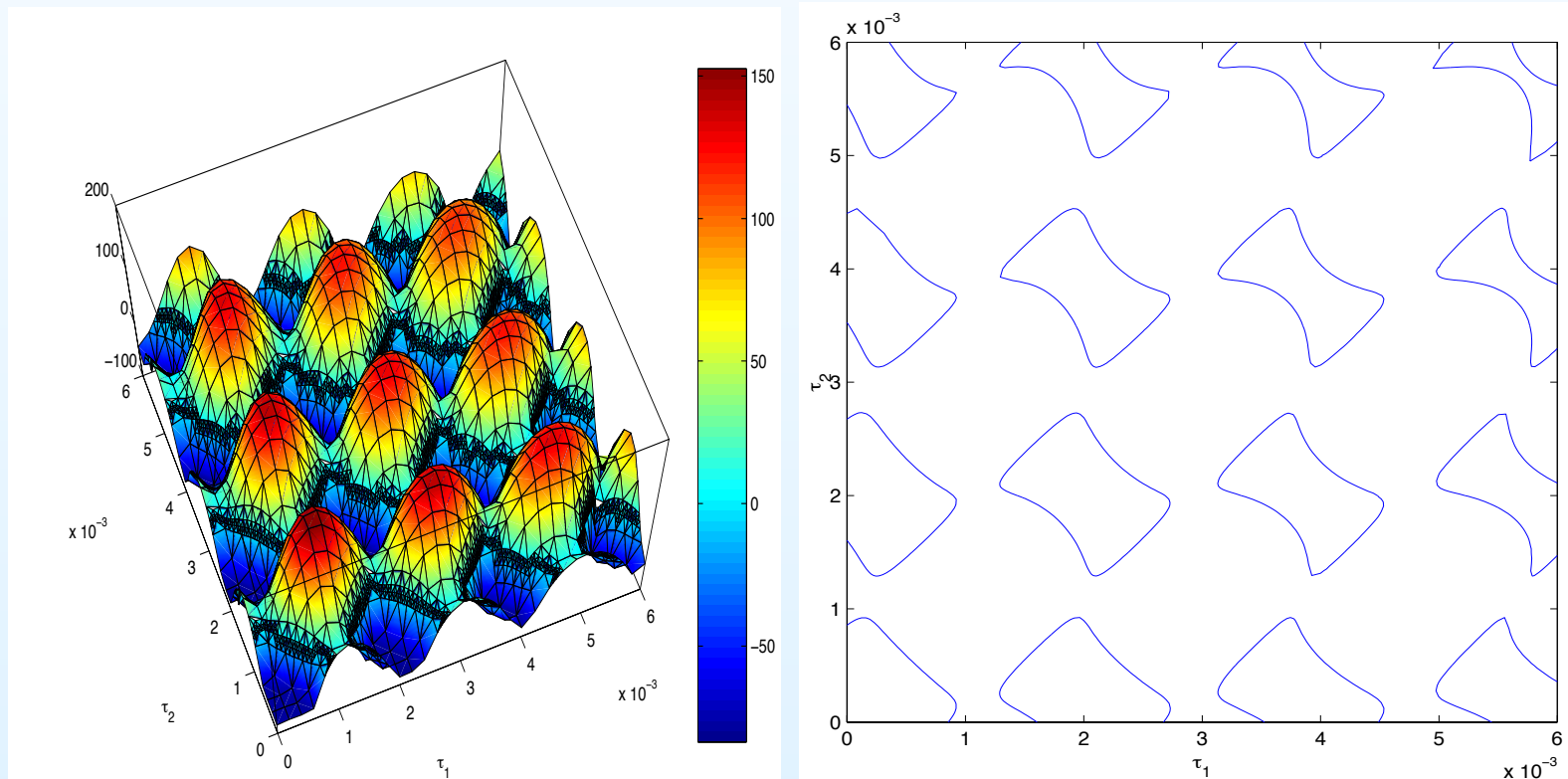




## Examples: multiple delays

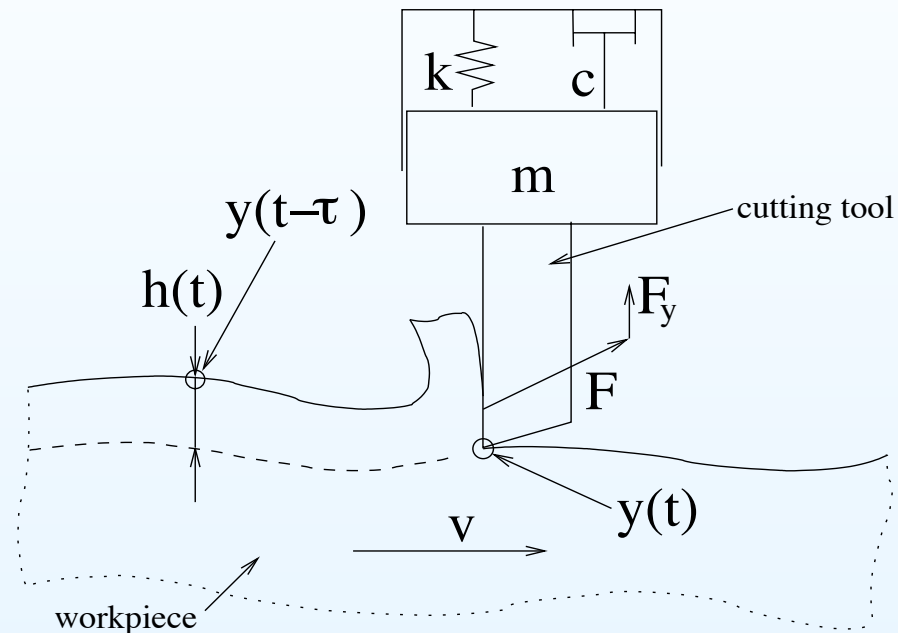
- consider the  $8d$  DDE

$$y'(t) = L_0 y(t) + L_1 y(t - \tau_1) + L_1 y(t - \tau_2) + L_2 y(t - 2\tau_1) + L_2 y(t - 2\tau_2) + L_3 y(t - \tau_1 - \tau_2), \quad L_i \in \mathbb{C}^{8 \times 8}$$



## Applications: metal cutting

- consider 1dof model of orthogonal metal cutting



$$y''(t) + 2\zeta\omega_n y'(t) + \omega_n^2 y(t) = \frac{F_y}{m}$$

## Applications: regenerative effect

- relative vibrations between tool and workpiece produces wavy surface

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---

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## Applications: regenerative effect

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- relative vibrations between tool and workpiece produces wavy surface
- after a round of the tool (or workpiece) chip thickness will vary
- cutting force depends on actual and delayed values of relative displacement between tool and workpiece
- this is called **regenerative effect**

## Applications: delay model

---

- with regenerative effect the model becomes

$$y''(t) + 2\zeta\omega_n y'(t) + \omega_n^2 y(t) = -\frac{K(t)w}{m}(y(t) - y(t - \tau))$$

- $K(t)$  possibly time periodic (e.g. milling process)

## Applications: delay model

- with regenerative effect the model becomes

$$y''(t) + 2\zeta\omega_n y'(t) + \omega_n^2 y(t) = -\frac{K(t)\omega}{m}(y(t) - y(t - \tau))$$

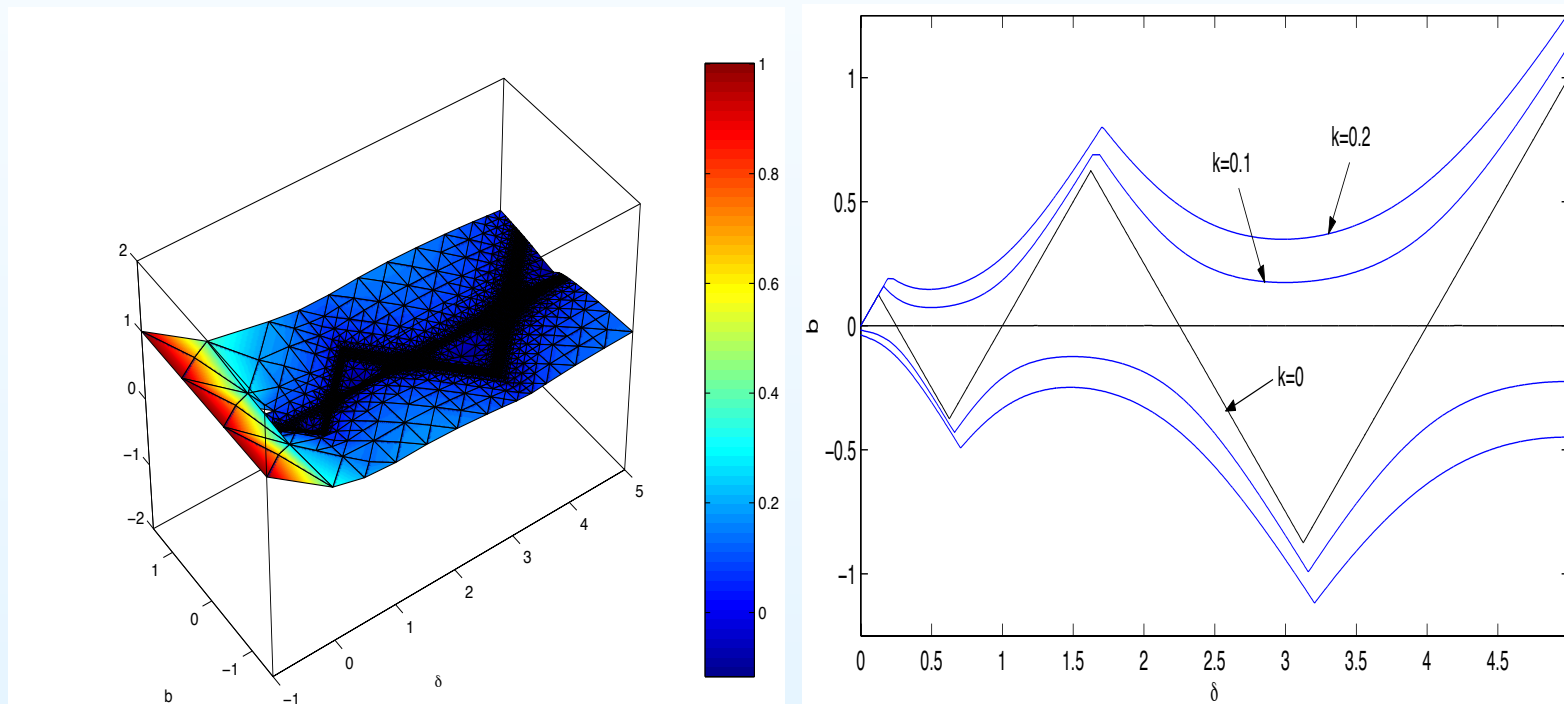
- $K(t)$  possibly time periodic (e.g. milling process)
- reduce to a model similar to the **damped delayed Mathieu equation**

$$y''(t) + ky'(t) + (\delta + \varepsilon \cos 2\pi t/T)y(t) = by(t - 2\pi)$$



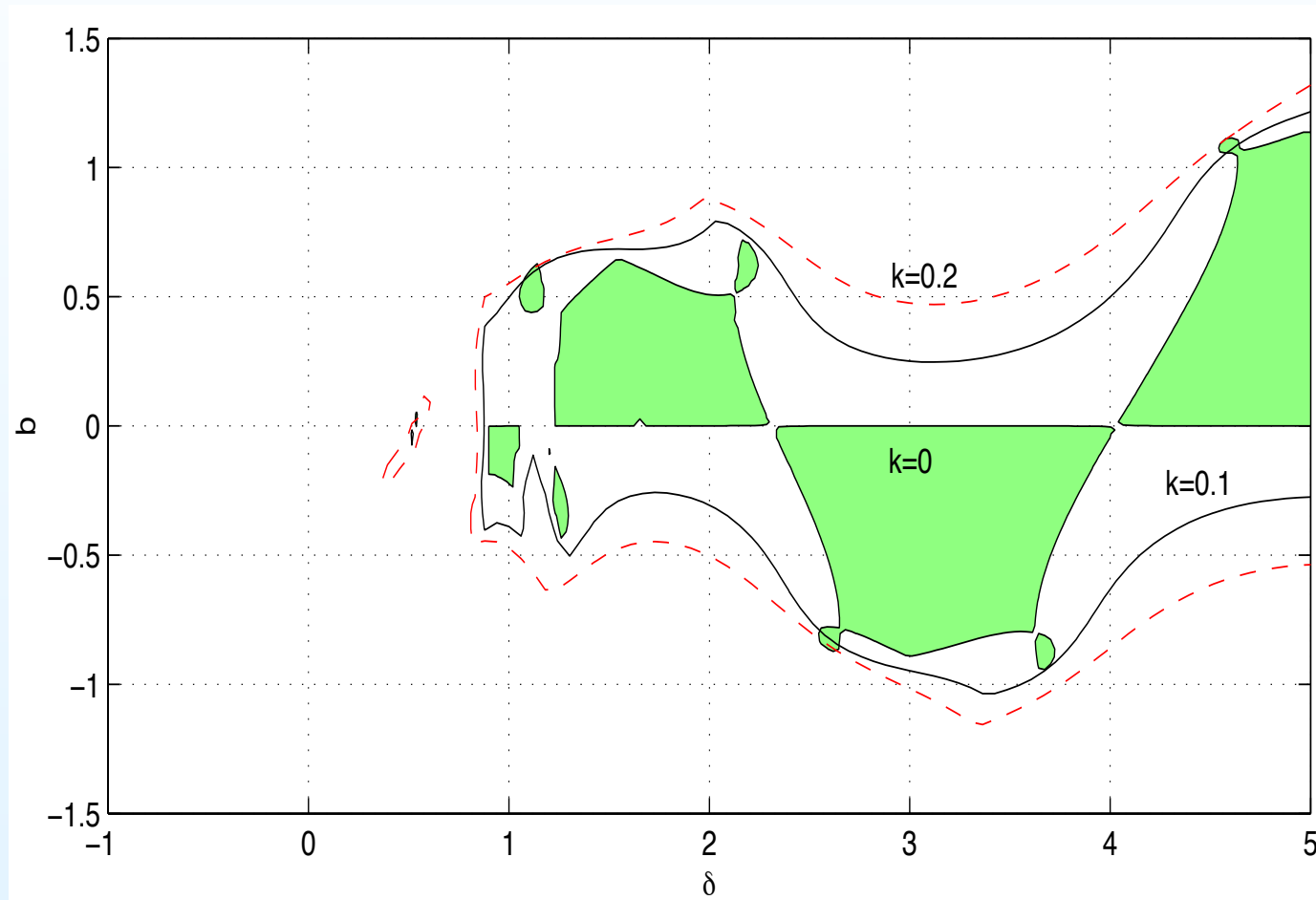
## Applications: stability chart

- consider  $\varepsilon = 0$ ,  $\delta$  and  $b$  as varying parameters
- Hsu-Bhatt-Vyshnegradskii stability chart



## Applications: periodic case

- consider the periodic case  $\varepsilon = 1$



## Conclusions

- increasing interest in time delay systems
- stability is an infinite dimensional problem

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- increasing interest in time delay systems
- stability is an infinite dimensional problem
- use numerical techniques to solve
- special attention to computational cost
- robust study of stability wrt varying parameters
- efficient computation of stability charts
- match best compromise among all tolerances

The end

*...and thanks for your attention!*